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## INDEX

Sr. No.	Title	Author	Subject	Page No.
1	Current Issues In Indian Capital Market	Bhavin S. Shah	Accountancy	1-3
2	Accounting Standard (AS) 30 Accounting for Financial Instruments	Kalola Rimaben A, Chauhan Lalit R.	Accountancy	4-6
3	A Study on Lithology and Petrography of the Tipam Sandstones Exposed along the Tipong Pani River Section of Upper Assam Basin	Dr. Pradip Borgohain	Applied Geology	7-11
4	Study of Fluvial Geomorphic Features of the Lower Subansiri Basin, North-East India using Remote Sensing and GIS.	Dr. Uttam Goswami	Applied Geology	12-14
5	Sheared volcanics in the north of Pugging, East Siang District, Arunachal Pradesh	T. K. Goswami, P. Bhattacharyya, D. Bezbaruah	Applied Geology	15-18
6	Heavy Metal Biosorption Using A Biopolymer Chitin	D. Saravanan, P. N. Sudha	Chemistry	19-23
7	Impact of peripheral cues on rural consumer buying decision for FMCG products with special reference to Palitana (Gujarat)	Dr K.S. Vataliya, Bhavik .P. Parmar	Commerce	24-26
8	A Growth of Rural Postal Life Insurance in India [ A Study with special Reference to Dharmapuri District]	Dr. A. Vinayagamoorthy K. Senthilkumar	Commerce	27-28
9	Promotional Strategies for International Markets with respect to Agricultural Products	Dr. B. B. Bhosale	Commerce	29-30
29	Business Risk And Financial Risk - Indian Corporate Sector	Dr. M. Dhanabhakyam, P. Balasubramanian	Commerce	31-33
10	"Customer Relationship Management"- In Banking Industry	G.V. Kori, Sri. Basavaraj Huggi	Commerce	34-36
11	Role of Investment Banks and Institutions in Economic Development	Jitendra Dhirajlal Karia, Dr. (Prof.) Vijay Kumar Soni	Commerce	37-38
12	Nature Of Information Shared And Communication Methods Used In Small Manufacturing Firms	Vipul Chalotra	Commerce	39-41
13	China's WTO Accession: An Empirical Assessment of Merchandise Trade with India	Anjali Tandon	Economics	42-45
14	Regional Disparities - Social Sector Expenditure in Rural-Urban India	Dr. Shankar B. Ambhore, Dr. Ashok S. Pawar	Economics	46-47
15	(Presenting Thought About Industry, Trade And Co-operation Of Rajarshri Shahu Maharaj)	Dr. Ashok Shankarrao Pawar, Dr.Sunita J. Rathod	Economics	48-49
16	An Assessment On Poverty Alliviation Programmes In Rural India-A Case Study	Dr. Parvathamma G. L.	Economics	50-55
17	Liveability in Guwahati: A Factor Analytic Approach	Dr. Daisy Das, Dr. Ratul Mahanta	Economics	56-58
18	Backward Class Disparities in higher Education in India	Dr. Shankar B. Ambhore, Dr. Pawar Ashok S.	Economics	59-60
19	Revenue and Expenditure Pattern of Municipal Corporations of Punjab	Naresh Kumar	Economics	61-66

20	Livelihood Security of Traditional Fishermen of Kerala: Analysing and Identifying the Roles of Self Help Groups	(Dr.) D. Rajasenan, Rajeev B.	Economics	67-70
21	Levels and Types of Questions Raised by EFL Teachers In Southern Al-Mazar Directorate of Education	Dr. Jihad Al-Turki	Education	71-74
22	Issues And Recommendations Of National Knowledge Commission In Higher Education System	Vidhi Bhalla	Education	75-77
23	Multiple Sequence Alignment of Different Species	Perna, Pankaj Bhambri, Dr. O.P. Gupta	Engineering	78-82
24	Analyzing the Phylogenetic Trees with Tree- building Methods	Jasmine, Pankaj Bhambri, Dr. O.P. Gupta	Engineering	83-85
25	Low Power High Speed with Improved Noise Margin for Domino CMOS Inverter.	Pushpa Raikwal, Dr.Vaibhav Neema, Dr.Sumant Katiyal	Engineering	86-88
26	Analysis of Drag for an Aircraft Wing Model with and without Winglet	Mitul Patel, Sharvil Shah, Dharmendra Dubey	Engineering	89-91
27	Cognitive Radio	Chauhan Jayesh R.	Engineering	92-95
28	Problems In Teaching English As A Compulsory Subject	Prof. Madhvi R. Acharya	English	96-97
30	Financial Banking Is The Science Of Managing Money: Indian Financial System	Dr. Shailesh N. Ransariya, Dr. Shailesh N. Ransariya	Finance	98-100
31	Carbon Trading a Step towards Green Environment	Ashok R. Bantwa	Finance	101-102
32	Effect of Supplementation of A Multinutrient Chocolate Bar on Nutritional Status and Athletic Performance	P. Muhtulakshmi, Dr. M. Sylvia Subapriya	Home Science	103-104
33	Imperatives of Inclusive Growth for Sustainable Development of Indian Economy Post Globalization	Dr Mahalaxmi Krishnan	Indian Economy	105-107
34	RIGHT TO INFORMATION ACT AND THE ROLE OF PRESS, MEDIA & NGO'S	Dr. Krushna Chandra Dalai	Law	108-109
35	``Thesis: A Powerful Source Of Information``	Arvind M Bhadrashetty	Library Science	110-111
36	Present Day English and Inflections	Dr Syed Mohammed Haseebuddin Quadri	Literature	112-113
37	Jigsaw II: An Effective Strategy To Develop Reading Comprehension Of High School Students	Dr. P. Nagaraj, Sindhu Thamba	Literature	114-115
38	CAPITAL STRUCTURE ANALYSIS (An Empirical Study of Paper Mills in India)	Ashok Mundhra	Management	116-118
39	Emerging Trends In Indian Rural Market	Dr. N. Ramanjaneyalu	Management	119-121
40	Credit Card Usage in Coimbatore	G. Murali Manokari, Dr. R. Ganapathi	Management	122-126
41	Micro Credit – Two Sides of the Same Coin	R. Durga Rani, J. Gnanadevan, Dr. R. Ganapathi	Management	127-130
42	Work Place Stress and Yoga Therapy	K. Revathi, Dr. R. Ganapathi	Management	131-132
43	Customer's Satisfaction Towards Modernized Petrol Stations With Reference to Coimbatore City	Dr. R. Ganapathi	Management	133-137

44	Evaluation Tactics: A tool to evaluate success of corporate training programme	Dr. Shobha Dedhia	Management	138-140
45	A Preliminary Study On Issues And Challenges Faced In Measurement Of Social Media Return On Investment	Khushbu Pandya	Management	141-142
46	Profitability Analysis (A Case Study of Selected Public and Private Sector Companies)	Manish Manglik	Management	143-144
47	Performance Management System	S.Jayakrishna, N.Sainath, M.V.Subbareddy, N.Raji Reddy	Management	145-147
48	A Study On Organizational Culture In Bharath Heavy Eletrical Limited, Ranipet	S.Sridhar, D.Yuvaraj, V. Kandasamy	Management	148-150
49	Cost Effective Transportation	Sarada Prasanna Patra Dr. Manjusmita Dash	Management	151-154
50	A Study On Efficiency Of Outbound Training With Reference to Titan Industries, Hosur	V. Kandasamy, D. Yuvaraj, S. Ragothaman	Management	155-157
51	Performance Improvement Enhance The Efficiency	Vidya L. Hulkund	Management	158-159
52	Packaging- The Salient Seller	Vidya L. Hulkund	Management	160-161
53	An Empirical Study Of Student Satisfaction With Reference To Gujarat Technological University (Gtu)	Dr. Vijay K. Patel	Management	162-163
54	Maximizing Customer Profitability in Retailing Industry (Durable Goods) - Role of Analytical CRM -A Case Analysis	Dr.A.R.Krishnan, R.Selvamani	Management	164-165
55	Financial Inclusion - Role Of Banking Industry	Dr. K. Marutha Muthu, Ms.T. A.Tamilselvi	Management	166-167
56	The Growth of Self Help Groups in India: A Study	S.Ravi, Dr. P. Vikkraman	Management	168-170
57	Role of E-Banking	K. K. Devi	Marketing	171-172
58	Reasons after the war of going Green –Green Marketing	Kavita A. Trivedi	Marketing	173-175
59	Strongly Minimal Generalized Boundary	K. Chandrasekhara Rao, P . Padma	Mathematics	176-177
60	ACCESSORY RENAL ARTERY: A CASE REPORT	Archana U Shekokar, Vandana A Tendolkardolkar	Medical Science	178-179
61	Fibrinous Pericarditis: A Case Report	Vandana A Tendolkar, Archana U Shekokar	Medical Science	180-181
62	Social life, Addictions and Subjective Wellbeing of the Transsexuals	Seemanthini.T.S, Manjula. M. Y	Psychology	182-184
63	Using E-Content In Science Class: The Effect Of Treatment, Gender, And Their Interaction On Science Achievement	Suman Rani	Psychology	185-188
64	Bullying - Societal Curse- A Serious Issue	Latha Janaki. R, Dr.Kalyani Kenneth	Social Science	189-191
65	Factor Influencing Foetal Wastage	Dr. Dipti Bhavsar, Dr. C. D. Bhavsar	Environment	192-195
66	Approach Of Universilization Educational And Women Empowerment Of Rajarshri Shahu Maharaj	Dr. Ashok Shankarrao Pawar, Dr. Sunita J. Rathod	Economics	196-199



## Analysis of Drag for an Aircraft Wing Model with and without Winglet

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**ABSTRACT**

*This work describes the aerodynamic characteristic for aircraft wing model with and without winglet. Rectangular wing and this aerofoil has been used to compare the result with previous research using winglet. The model of the rectangular wing with winglet has been fabricated using polystyrene before design using CATIA software and finally fabricated in wood. The experimental analysis for the aerodynamic characteristic for rectangular wing without winglet, wing with horizontal winglet and wing with 60 degree inclination winglet for Reynolds number  $1.66 \times 10^5$ ,  $2.08 \times 10^5$  and  $2.50 \times 10^5$  have been carried out in open loop low speed wind tunnel at the Aerodynamics laboratory in Bhagwant university, Ajmer. The experimental result shows 25-30 % reduction in drag coefficient and 10- 20 % increase in lift coefficient by using winglet for angle of attack of 8 degree.*

**Keywords : Aerofoil, Wind tunnel, Winglet, Drag Coefficient**

**I. INTRODUCTION**

One main obstacles limiting the performance of aircraft is the drag that the aircraft produces. This drag stems out from the vortices shed by an aircraft's wings, which causes the local relative wind downward (an effect known as downward) and generated a component of the local lift force in the direction of the free stream called induced drag. The strength of this induced drag is proportional to the spacing and radii of these vortices. By designing wings which force the vortices farther apart and at the same time create vortices with large core radii, one may significantly reduce the amount of the drag the aircraft induces. Airplanes which experience less drag require less power and therefore less fuel to fly an arbitrary distance, thus making flight, commercial and otherwise, more efficient and less costly. Vortices at the wing tip can cause crash in aircraft. This is when a big aircraft goes in front of a small aircraft; this big aircraft which has larger vortices can cause the small aircraft to loose control and crash. In airport to minimize the separation rule, an aircraft of a lower wake vortex category must not be allowed to take off less than two minutes behind an aircraft of a higher wake vortex category.

**METHODOLOGY**

**A. Wind tunnel, Instrumentation and model details.**

The aircraft model's wing with two sets of bird feather like winglet has been designed and fabricated using wood for aerodynamic characteristic analysis in subsonic wind tunnel at Aerodynamic Laboratory, University Putra Malaysia. The NACA 653-218 airfoil has been used for the structure of wing, winglet and adapter. The winglet design is shown in Fig. 1.

The aircraft wing model has a span of 0.66 m and a chord of 0.121 m as shown in Fig. 2.

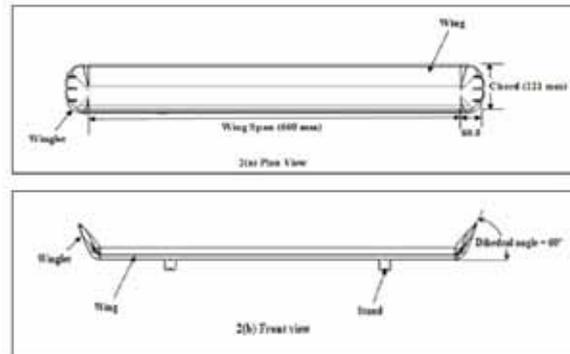
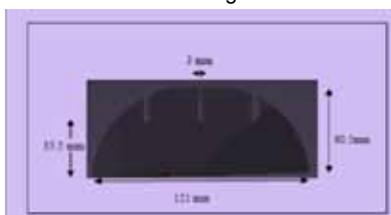


Fig.2. Rectangular Wing with Winglet using Adapter

**B. Theoretical Models**

Lift Coefficient and Drag coefficient are defined as [19-20]



$$C_L = \frac{L}{\frac{1}{2} \rho_{\infty} V_{\infty}^2 S}$$

$$C_D = \frac{D}{\frac{1}{2} \rho_{\infty} V_{\infty}^2 S}$$

$\rho^\infty$  is the air density in kg/m<sup>3</sup>,  $V^\infty$  is the free stream velocity in m/s,  $c$  is the chord length in m and  $S$  is the reference area in m<sup>2</sup>.

Using equation of state of perfect gas the air density kg/m<sup>3</sup> is defined as

$$\rho_\infty = \frac{p}{RT}$$

Where,  $p$  is the absolute pressure in N/m<sup>2</sup>,  $T$  is the temperature in K, and  $R$  is the gas constant of air in Nm/(kg) (K).

Reynolds number based on the chord length is defined as

$$Re = (\rho^\infty v^\infty c)/\mu$$

Where,  $v^\infty$  is the free stream velocity in m/s;  $\mu$  is the dynamic viscosity in kg/(m)(s) and  $c$  is the chord length in m.

The air viscosity,  $\mu^\infty$  is determined using Sutherland's equation describe below

Where,  $T$  is the temperature in K.

**C. Experimental Procedure**

Experiments were conducted in the Aerodynamics Laboratory Faculty of Engineering (University Putra Malaysia) with subsonic wind tunnel of 1 m x 1 m rectangular test section and 2.5 m long. The wind tunnel could be operated at a maximum air speed of 50 m/s and the turntable had a capacity for setting an angle of attack of 14 degree. The ambient pressure, temperature and humidity were recorded using barometer, thermometer, and hygrometer respectively for the evaluation of air density in the laboratory environment. Fig. 3 shows a photograph of the aircraft wing model with winglet, which is mounted horizontally in the test section of the wind tunnel.

Fig.3. Schematic diagram of the wing with winglet

The tests were carried out with free-stream velocity of 21.36 m/s, 26.76 m/s, and 32.15 m/s respectively with and without winglet of different configurations. The coefficient of lift (Table I) and coefficient of drag (Table II) were obtained from the experimental results as per the procedure explained in [16-17]. The simulations on the parameters were conducted at Reynolds numbers 1.7x10<sup>5</sup>, 2.1x10<sup>5</sup>, and 2.5x10<sup>5</sup> respectively by using the MATLAB.

**D. Calibration of External Balance**

Calibration of the six-component balance has been done to check the calibration matrix data provided by the manufacturer. Fig. 4 shows a photograph of the calibration rig used for the validation of calibration matrix, which is mounted on the upper platform of the balance in place of model. The relationship between signal readings,  $L_i$  and the loads,  $F_i$  applied on the calibration rig are given by the following matrix equation, the detailed procedure of calibration using Matlab software is explained elsewhere [17-18].

$$\{L_i\} = [K_{ij}]\{F_i\}$$

Where,  $[K_{ij}]$  is the coefficient matrix,  $\{L_i\}$  is the signal matrix,

Lift Coefficient Data				
Winglet Configuration	Reynolds Number 10 <sup>5</sup>	Lift coefficient CL		
		Initial angle of attack 0o	Stall angle of attack 8o	Final angle of attack 14o
Without winglet	1.6	0.227	0.803	0.665
	2.0	0.255	0.786	0.588
	2.4	0.307	0.879	0.734

Configuration 1 (0o angle)	1.6	0.403	0.848	0.570
	2.0	0.431	0.913	0.720
	2.4	0.412	0.970	0.757
Configuration 2 (6o angle)	1.6	0.443	0.994	0.781
	2.0	0.457	0.957	0.751
	2.4	0.482	0.991	0.829

Table II				
Drag Coefficient Data				
Winglet Configuration	Reynolds Number 10 <sup>5</sup>	Drag coefficient CD		
		Initial angle of attack 0o	Stall angle of attack 8o	Final angle of attack 14o
Without winglet	1.6	0.087	0.155	0.257
	2.0	0.084	0.151	0.288
	2.4	0.066	0.135	0.217
Configuration 1 (0o angle)	1.6	0.060	0.101	0.191
	2.0	0.053	0.092	0.162
	2.4	0.051	0.083	0.129
Configuration 2 (6o angle)	1.6	0.077	0.119	0.194
	2.0	0.065	0.105	0.162
	2.4	0.053	0.140	0.160

The calibration matrix is obtained by finding the inverse of  $K_{ij}$ , coefficient matrix and it compares well with the calibration matrix data supplied by the manufacturer with six component external balance.

**E. Speed Calibration**

The airflow velocity was controlled by the RPM controller of the wind tunnel. For the different Hz settings at the RPM controller the flow velocities in wind tunnel test section were recorded using six-component external balance software. The validity of the digital manometer was confirmed by comparing the dynamic pressure measured through the digital manometer and through the tube manometer used along with the pitot tube mounted in the test section. The experimental error using the external balance was nearly 6% [16, 21]. The flow velocity readings of the external balance are corrected through the following calibration equation obtained through the data shown in Fig.5,

$$y = 1.0796x - 0.2336 \quad (7)$$

Where  $x$  denotes external balance software velocity (m/s) and  $y$  denotes digital manometer velocity (m/s).

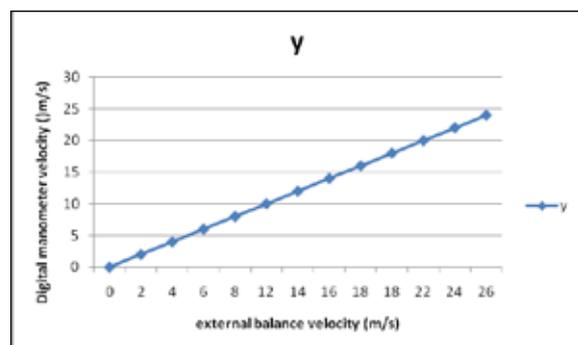


Fig.4. Flow velocity calibration for external balance

Using the equation (7), the actual value of free stream air velocity would be 21.36 m/s for corresponding 20 m/s of air velocity from six-component external balance software.

**III. RESULTS AND DISCUSSIONS**

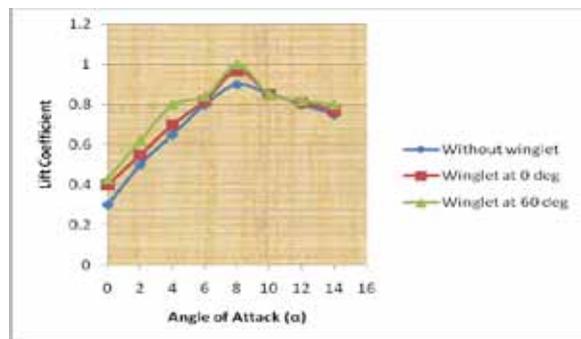
**A. Test Conditions**

The aircraft model tests with different configuration of winglets and without winglet were carried out at Reynolds numbers  $1.7 \times 10^5$ ,  $2.1 \times 10^5$ , and  $2.5 \times 10^5$ . The measured values for the lift force, and drag force for the various configurations were given in Ref. [16-17] and coefficient of lift and coefficient of drag were calculated as per the procedures explained.

**B. Coefficient of Lift**

The coefficient of lift versus angle of attack for the aircraft wing model with and without winglet studied in the present investigation are shown in Fig. 7 for the maximum Reynolds number of  $2.5 \times 10^5$ . From the figure it is observed that the lift increases with increase in angle of attack to a maximum value and thereby decreases with further increase in angle of attack

Fig.5. Lift Coefficients for the Wing Model



**B. Coefficient of Drag**

The drag coefficients of the aircraft wing model under test for all Reynolds numbers are shown in Fig. 8. From the graph, it is observed that the drag coefficient for the aircraft wing model measured under all the configurations under this study shows an increasing trend with angle of attack for a Reynolds number  $0.25 \times 10^6$ . The drag increases slowly with increase in angle of attack to a certain value and then it increases rapidly with further increase in angle of attack. The rapid increase in drag coefficient, which occurs at higher values of angle of attack, is probably due to the increasing region of separated flow over the wing surface, which creates a large pressure drag. From the figure it is observed that the values of the minimum drag coefficients are 0.067, 0.053, and 0.052 respectively for different configurations for the maximum Reynolds number of  $2.5 \times 10^5$  which occur at zero angle of attack. In particular the measured drag values against the angle of attack are minimum for the winglet of configuration 1 and 2 over

the values of the range of angle of attack considered under this study. To establish the superiority of the winglet at 0 degree over the winglet at 60 degree more detailed experiments are required.

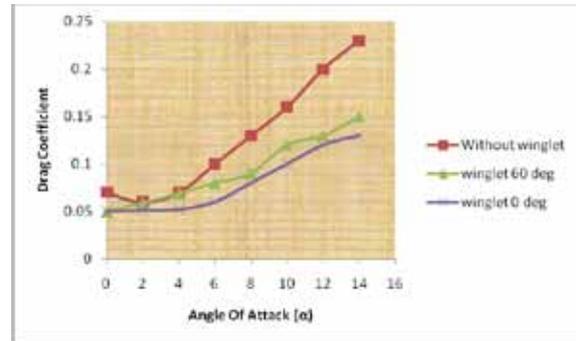


Fig.6. Drag Coefficients for the Wing model of an aircraft

**D. Lift/Drag ratio Characteristics**

The lift/drag ratio is the outcome of the observations made in the two preceding sections. It is observed from the Fig. 9 that the lift/drag ratio for all the configurations considered increases with an angle of attack to its maximum value and thereby it decreases with further increase in angle of attack for a Reynolds number  $2.5 \times 10^5$ .

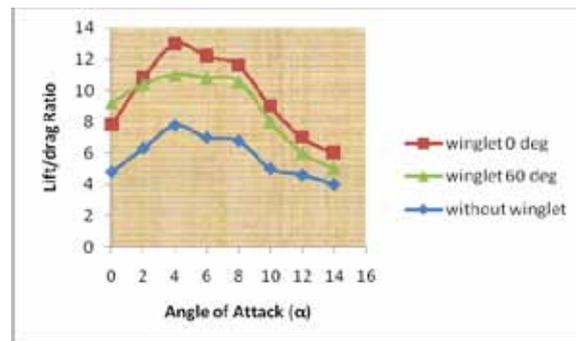


Fig.7. Lift/Drag ratio for the Wing model of an aircraft

**CONCLUSION**

The conclusions drawn from this investigation is that the drag coefficient and lift coefficient graph it is clearly shown that using winglet will increase lift force and reduce drag force. This winglet design is capable to reduce induced drag force and convert wing tip vortices to additional thrust which will save cost by reducing the usage of fuel, noise level reduction and increase the efficiency of the aircraft engine. The experiment result shows 25-30 % reduction in drag coefficient and 10-20 % increase in lift coefficient by using winglet for angle of attack of 8 degree

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